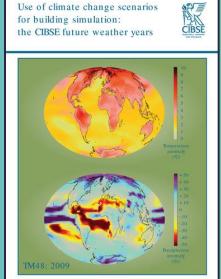
How Can We Improve Building Thermal Simulation Software



Ant Wilson

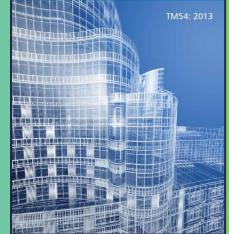


Use of climate change scenarios

for building simulation:

Evaluating operational energy performance of buildings at the design stage

CIBSE



Design for improved solar

shading control

TM37: 200

Director/AECOM Fellow

Building Engineering



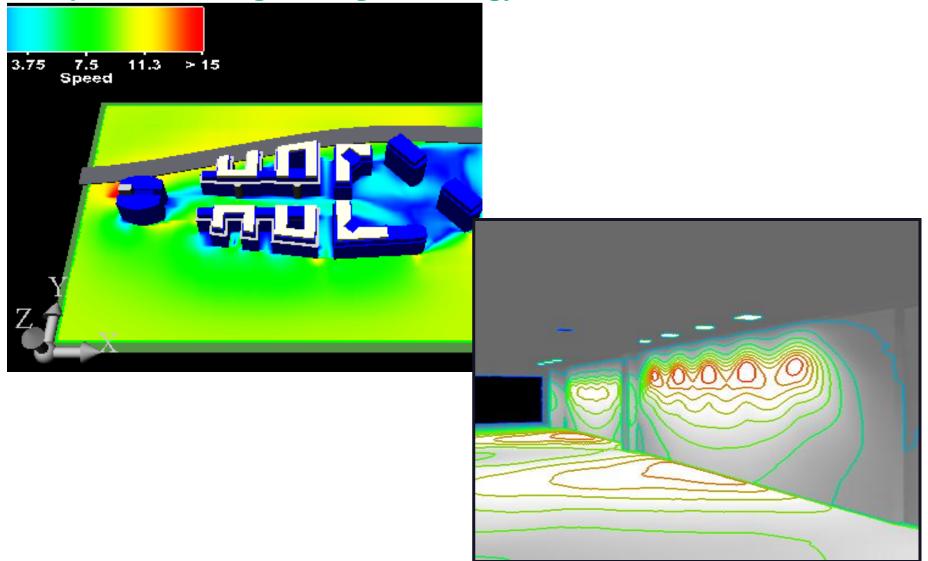








Computer Modelling – Design or Energy Simulation

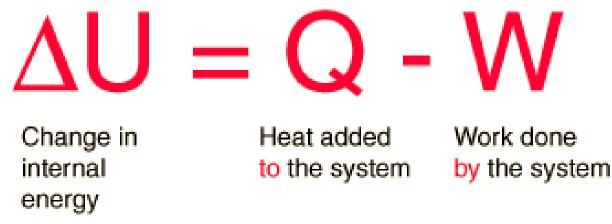




First Law of Thermodynamics

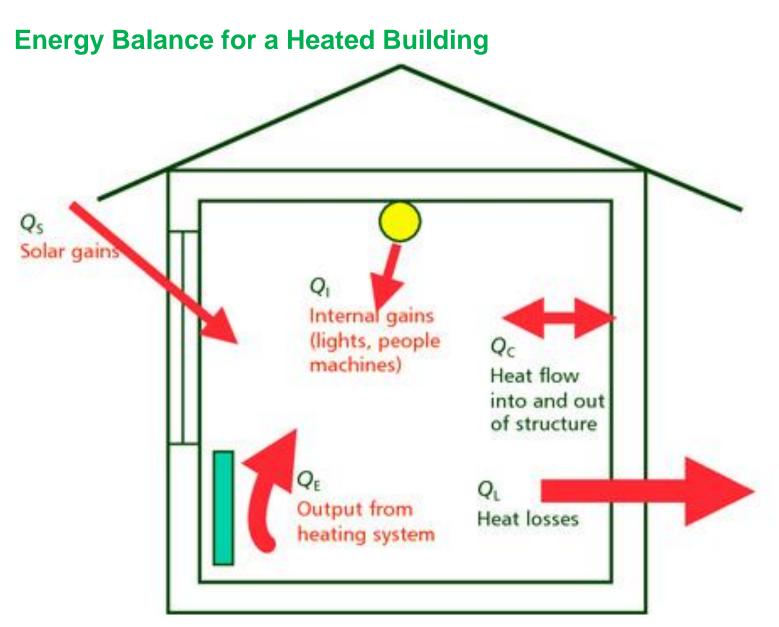
The first law of thermodynamics is the application of the conservation of energy principle to heat and thermodynamic processes:

The change in internal energy of a system is equal to the heat added to the system minus the work done by the system.





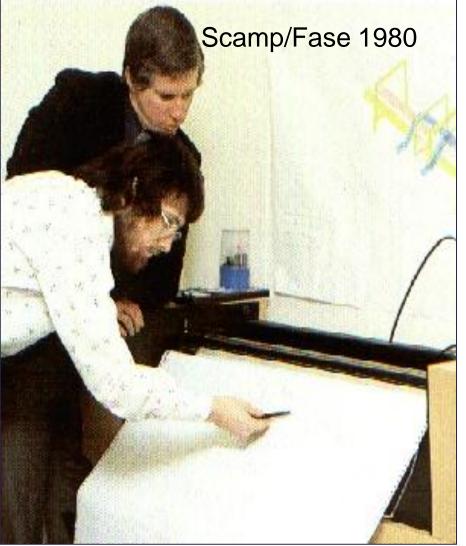


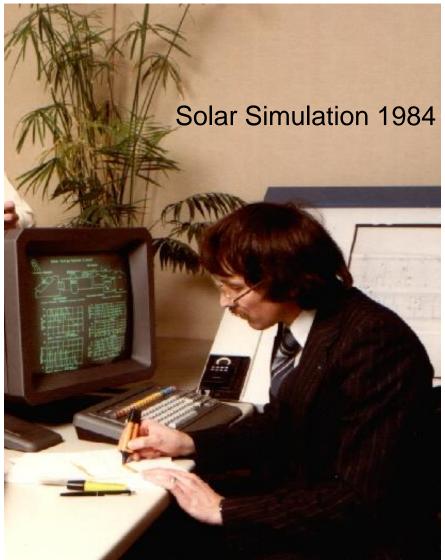






The Early Days – Faber Computer Operations

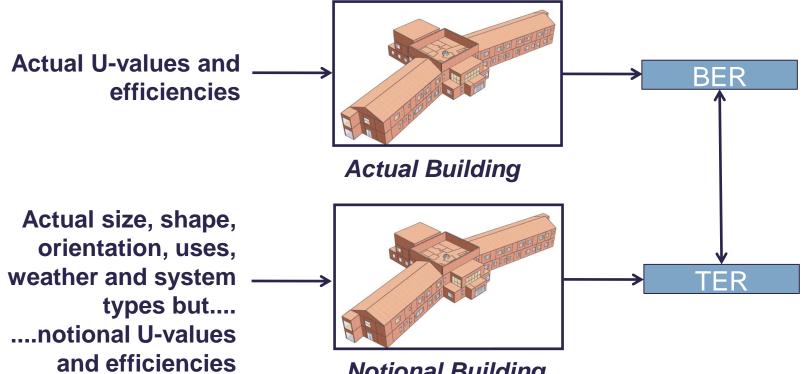








Cost / Benefit Analysis Used to Determine Target Concurrent Notional Recipe Approach

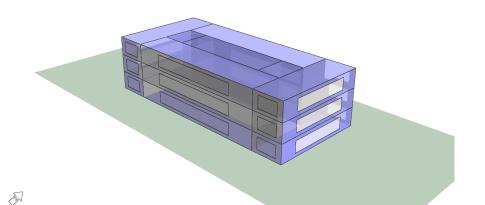


Notional Building

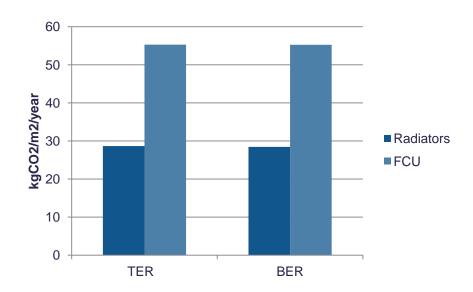
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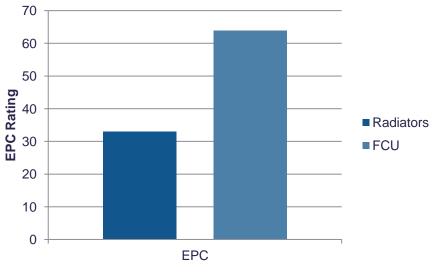


Impact of HVAC selection on EPC Rating



- 2100m² office building
- Two models:
 - 1. Radiator heated only
 - 2. Fan Coil Units
- Both models 'just-comply' with Building Regulations Part L2006

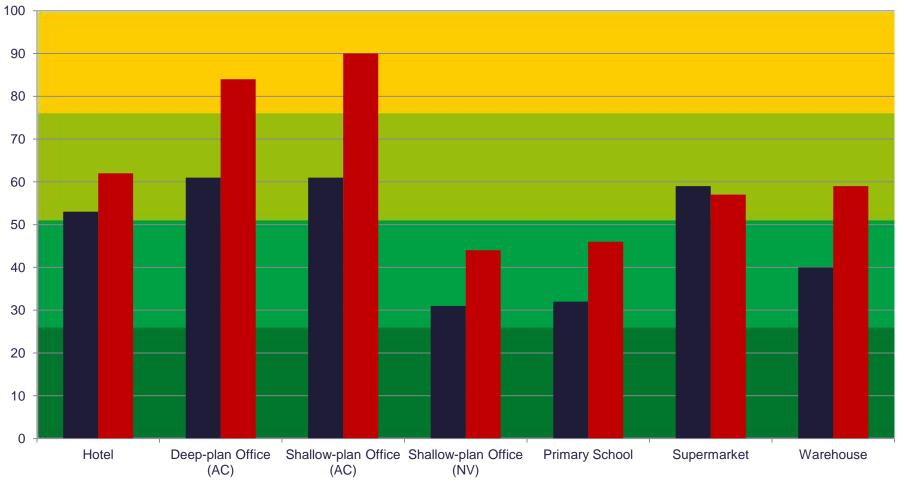




7

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Operational Ratings for Typical Buildings when run with NCM Templates

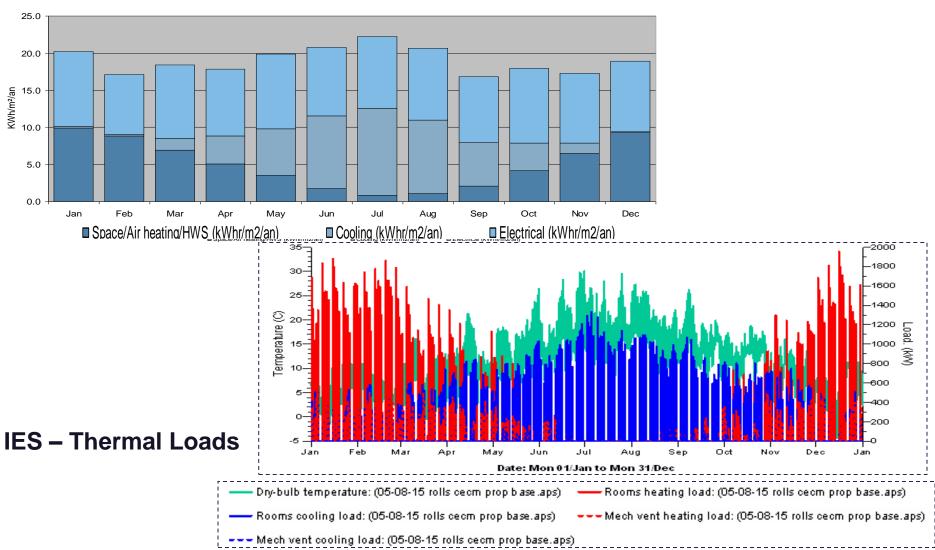






Building Energy Loading

9



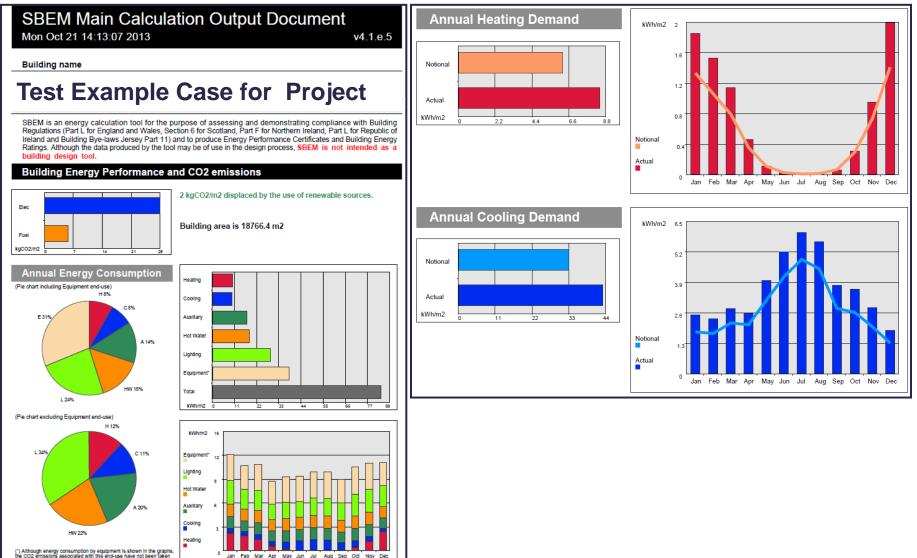
Building Energy Requirement (kWh/m²/an)

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SBEM Main Calculation Output



 10^{-}

into account when producing the rating.





BRUKL Output Document

BRUKL Output Document

HMGovernment

Compliance with England and Wales Building Regulations Part L 2010

Criterion 1: The calculated CO₂ emission rate for the building should not exceed the target

The building does not comply with England and Wales Building Regulations Part L 2010

1.1	CO ₂ emission rate from the notional building, kgCO ₂ /m ² .annum	27.1
1.2	Target CO ₂ emission rate (TER), kgCO ₂ /m ² .annum	27.1
1.3	Building CO ₂ emission rate (BER), kgCO ₂ /m ² .annum	31.3
1.4	Are emissions from the building less than or equal to the target?	BER > TER
1.5	Are as built details the same as used in the BER calculations?	Separate submission

Criterion 2: The performance of the building fabric and the building services should achieve reasonable overall standards of energy efficiency

2.a Building fabric

Element	Ua-Limit Ua-Calo UI-Calo			Surface where the maximum value occurs*					
Wall**	0.35	0.2	0.2	GFBM0000_W21					
Floor	0.25	0.14	0.22	1VD_0001_F_5					
Roof	0.25	0.22	0.22	GFRC0000_C_5					
Windows***, roof windows, and rooflight	s 2.2	1.01	1.3	GFRT0000_W3-W0					
Personnel doors	2.2 "No external personnel doors"								
Vehicle access & similar large doors	similar large doors 1.5 "No external vehicle access doors"								
High usage entrance doors	gh usage entrance doors 3.5 "No external high usage entrance doors"								
U=Limit = Limiting area-weighted average U-values [W/(m ² K)] U=cate = Calculated area-weighted average U-values [W/(m ² K)] U=Cate = Calculated maximum individual element U-values [W/(m ² K)]									
* There might be more than one surface where the maximum U-value occurs. ** Automatic U-value check by the tool does not apply to curtain walls whose limiting standard is similar to that for windows. *** Display windows and similar glazing are excluded from the U-value check. N.B.: Neither roof ventilators (inc. smoke vents) nor swimming pool basins are modelled or checked against the limiting standards by the tool.									
Air Permeability Worst acceptable standard This building									

Air Permeability	worst acceptable standard	This building
m ^s /(h.m ²) at 50 Pa	10	10





Four Key Areas That Can Be Improved

Climate data

Occupancy and internal heat gains

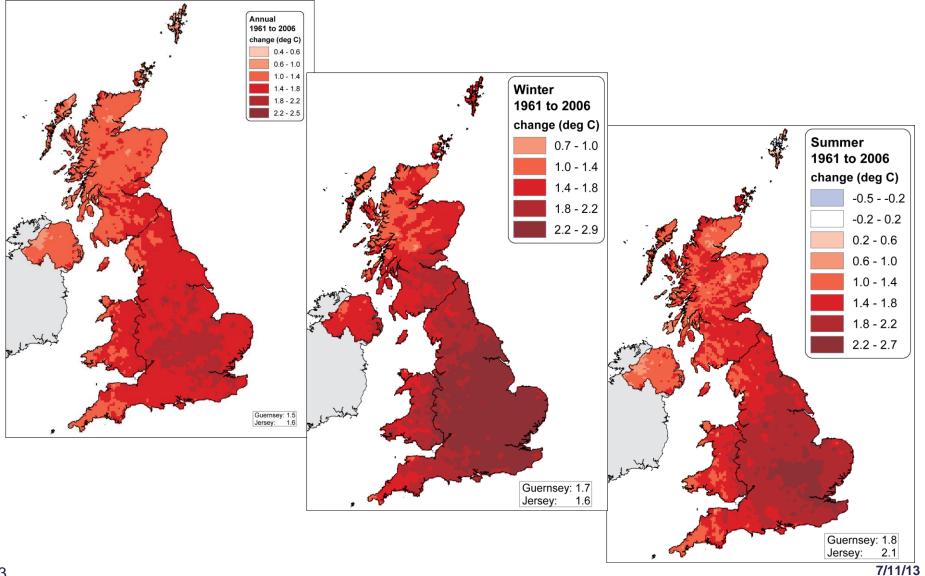
System performance

Thermal properties of building materials



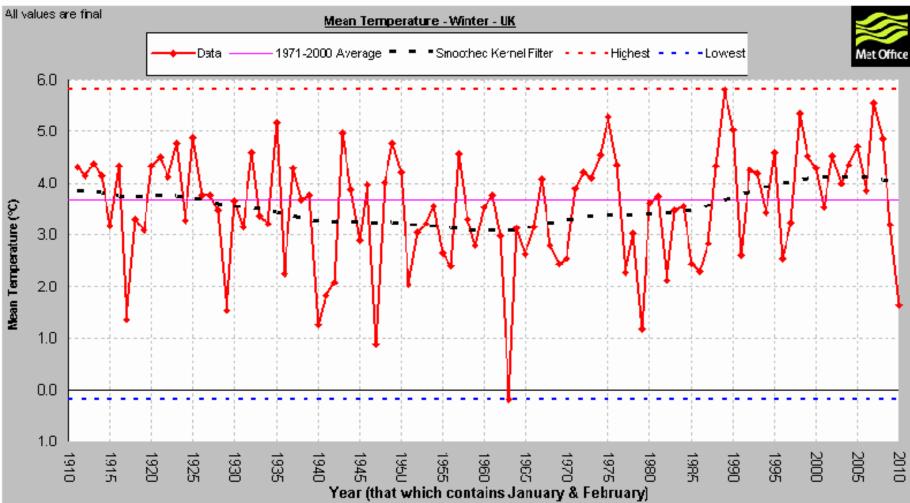


Changes in Average Temperatures from 1961 to 2006





Mean UK Winter (January and February) Temperatures from 1910 - 2010







UK Weather Statistic for 2010 With Coldest December

Ireland

Provisional 2010	Mean te C)	emperature (deg	Sunshine o		Precip	oitati	ion								
	Actual	Difference from normal (71-00)	Actual (hours)	n			(mm) no		Percentage of normal (71-00) (%)						
UK	8.0	-0.6	1477.2	108			940.1 83		83						
England	8.8	-0.6	1578.7	109			722.2	2.2 86							
Wales	8.2	-0.7	1612.6	116			1118.	8.3 78							
Scotland	6.5	-0.7	1277.3	107			1233.	1233.8 81							
Northern Ireland	8.0	-0.7	1442.9 Provisional	116		116 Mean temperatur		emperature	1047. (dea		94				
Treating			Dec 2010		C)	Simporataro	laca	Sur	ishine d	luration		Precipitat	tion		
					Actual	Difference normal (71		Acti (ho	ual urs)	Percentage normal (71 (%)		Actual (mm)	Pero nori (%)		
			UK		-1.0	-5.2	53.4		4	139		47.4	38		
			England		-0.5	-5.2	52.		6	118	18		38		
			Wales		-0.4	-5.2		61.	3	159		53.0	31		
			Scotland		-1.9	-5.0	48		2	167		63.1	37		
			Northern		-0.6	-5.4	78.7 2		232		66.5	56			

Provisio 2010

Percentage of

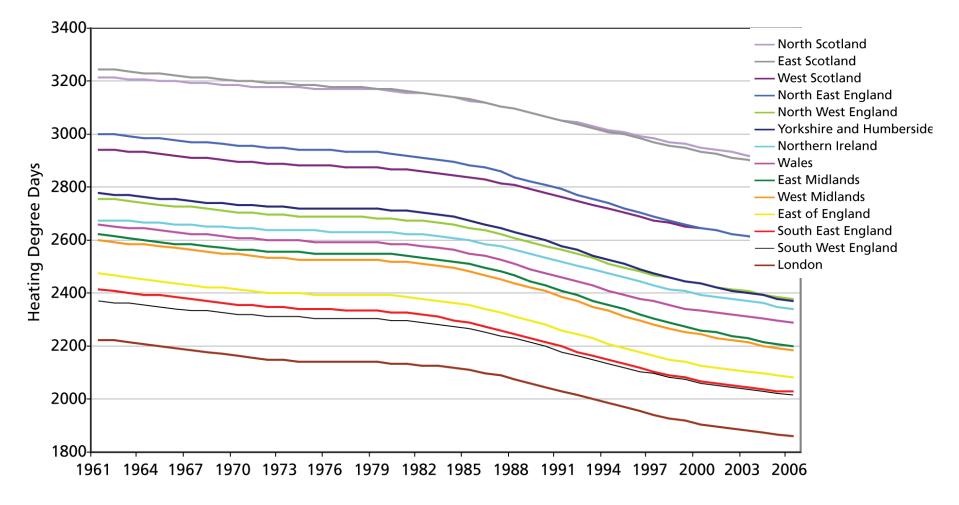
normal (71-00)

(%)





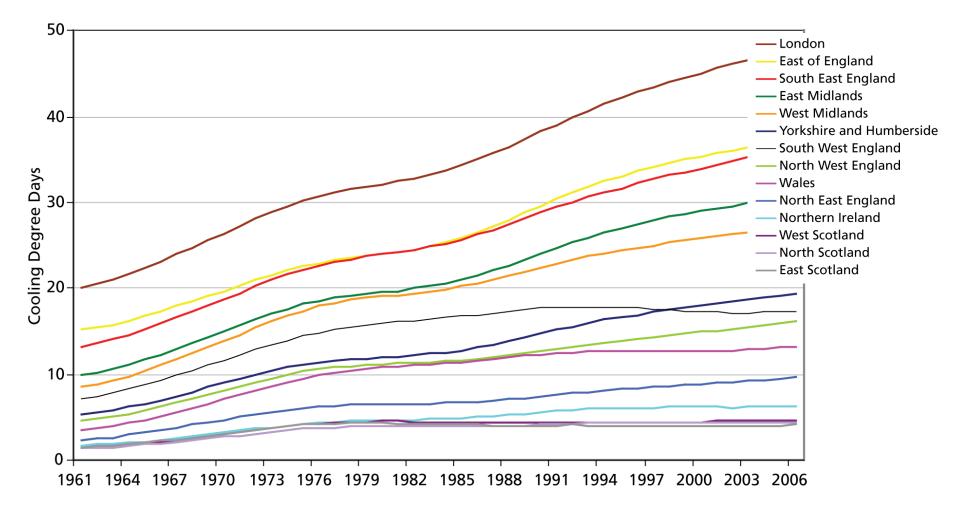
Reduction in Heating Demand from Weather over 45 Years



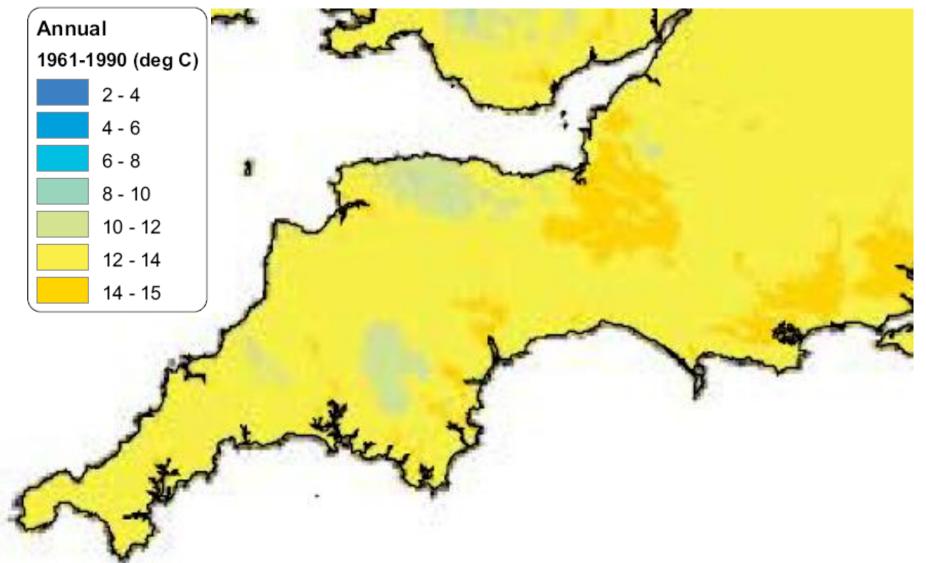




Increase in Cooling Demand from Weather over 45 Years



Average Temperatures in the South West

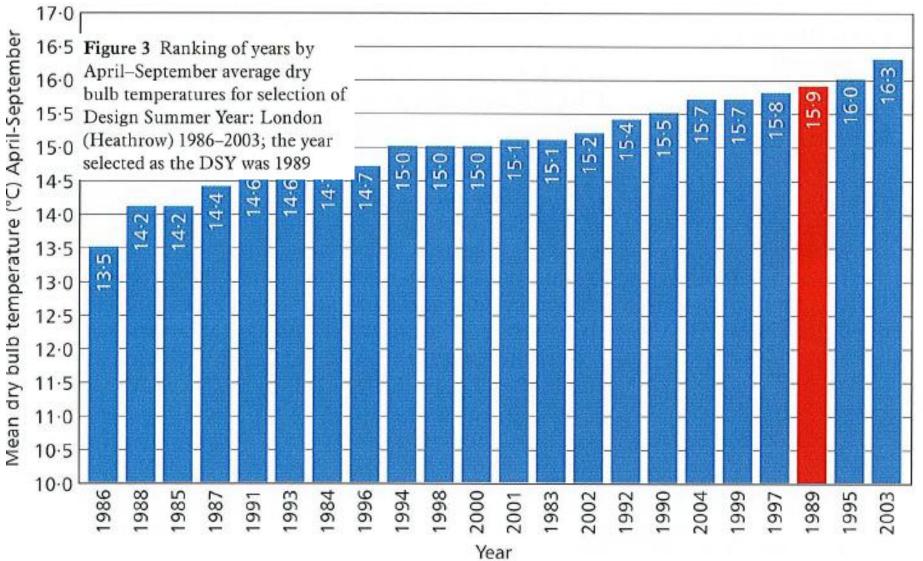


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CIBSE Design Summer Year Data







Highest and Lowest Temperature Changes by 2080

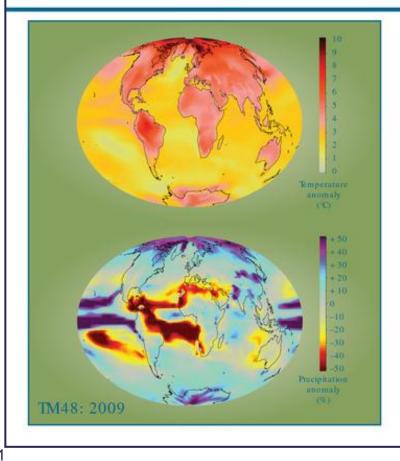
Variable		tem	Mean temperature, winter			Mean temperature, summer			Mean daily maximum temperature, winter			Mean daily maximum temperature, summer			Mean daily minimum temperature, winter			Mean daily minimum temperature, summer		
Probability	level	10%	50%	90%	10%	50%	90%	10%	50%	90%	10%	50%	90%	10%	50%	90%	10%	50%	90%	
High emissions	Highest change in UK	2.2	3.8	5.8	2.9	5.3	8.4	1.6	3.4	6.1	3.0	6.8	11.7	2.0	4.2	7.0	2.8	5.3	8.8	
	Lowest change in UK	1.0	2.1	3.5	1.6	3.1	5.0	1.1	2.3	3.9	1.2	3.5	6.3	0.8	2.4	4.3	1.7	3.3	5.6	
Medium emissions	Highest change in UK	1.7	3.1	4.8	2.2	4.2	6.8	1.3	2.9	5.1	2.2	5.4	9.5	1.5	3.5	5.9	2.0	4.1	7.1	
	Lowest change in UK	0.8	1.8	3.1	1.2	2.5	4.1	0.8	2.0	3.4	1.1	2.8	5.0	0.6	2.1	3.7	1.3	2.7	4.5	
Low emissions	Highest change in UK	1.5	2.7	4.1	1.4	3.1	5.3	1.3	2.6	4.3	1.4	4.1	7.5	1.4	2.9	4.8	1.4	3.2	5.6	
	Lowest change in UK	0.8	1.7	2.7	0.8	1.9	3.2	0.9	1.8	3.0	0.7	2.1	3.9	0.7	2.0	3.3	0.9	2.1	3.5	





CIBSE TM48: 2009

Use of climate change scenarios for building simulation: the CIBSE future weather years

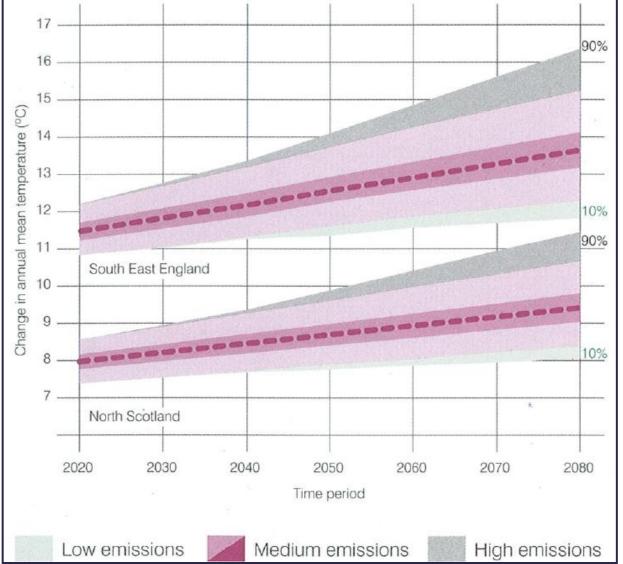


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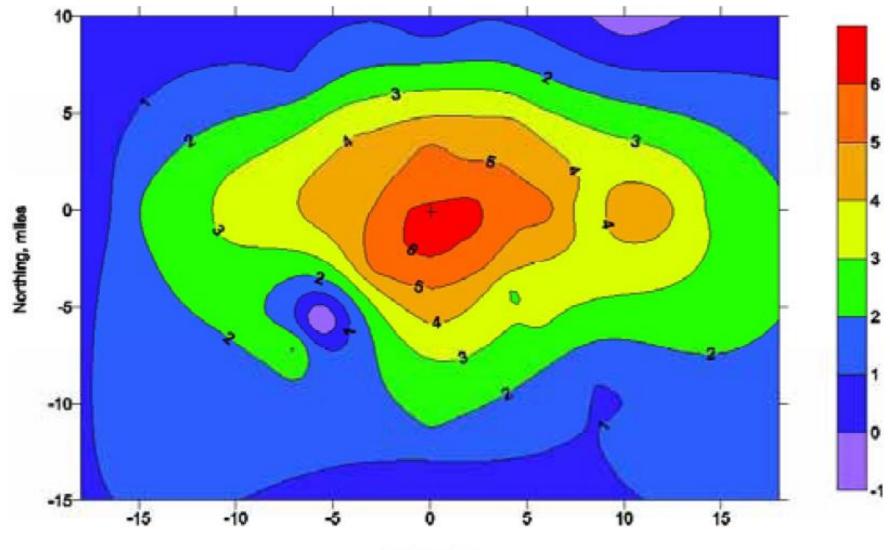


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Temperature Heat Island Effect in London

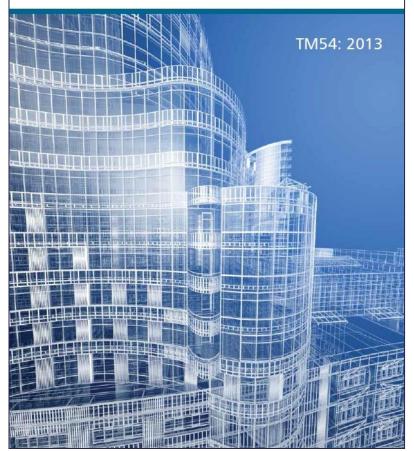


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Purpose of CIBSE TM54: 2013

Evaluating operational energy performance of buildings at the design stage

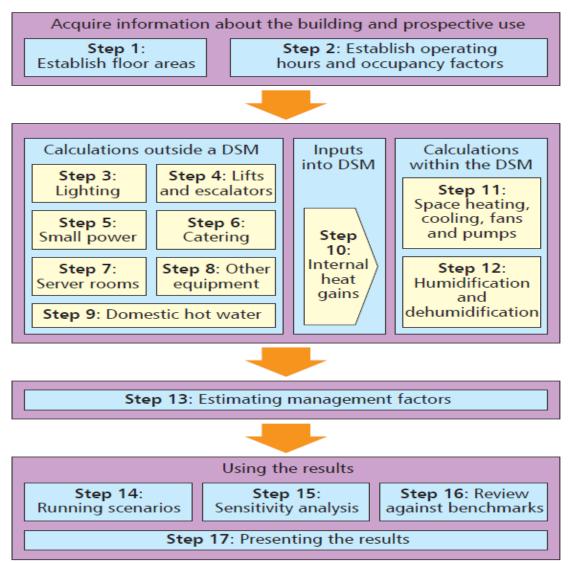


- Provide a methodology to calculate operational energy use
- Demonstrate that energy performance is dependent on how the building is occupied, run and maintained, as well as how it is designed and constructed.

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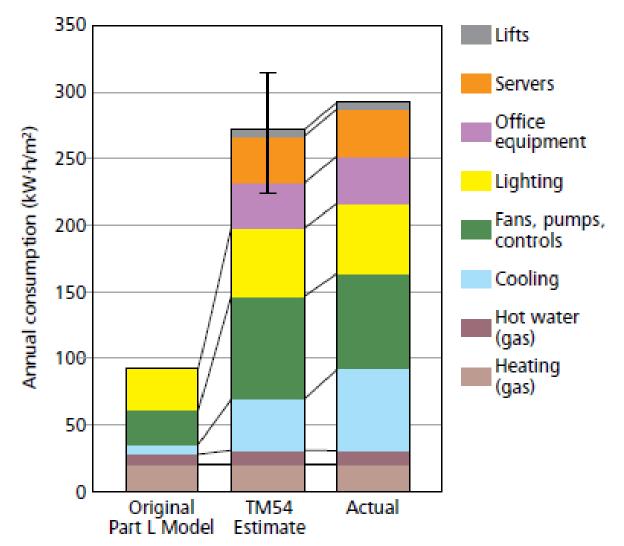
Methodology Within CIBSE TM54: 2013





CIBSE TM54: 2013 Estimate of Annual Energy Consumption

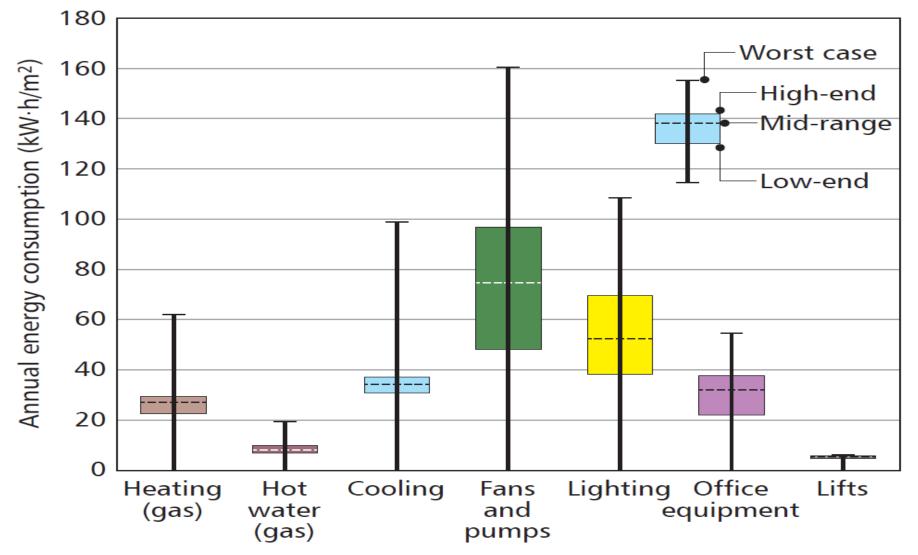
Part L model versus TM54 estimate versus actual







Running Scenarios following CIBSE TM54: 2013

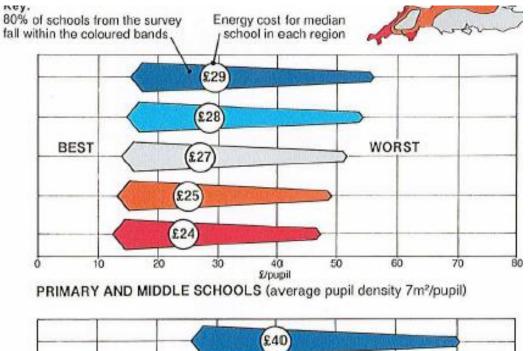


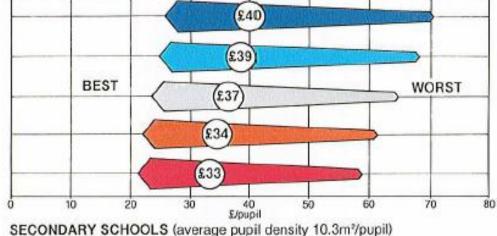




Schools Old Energy Consumption Guide



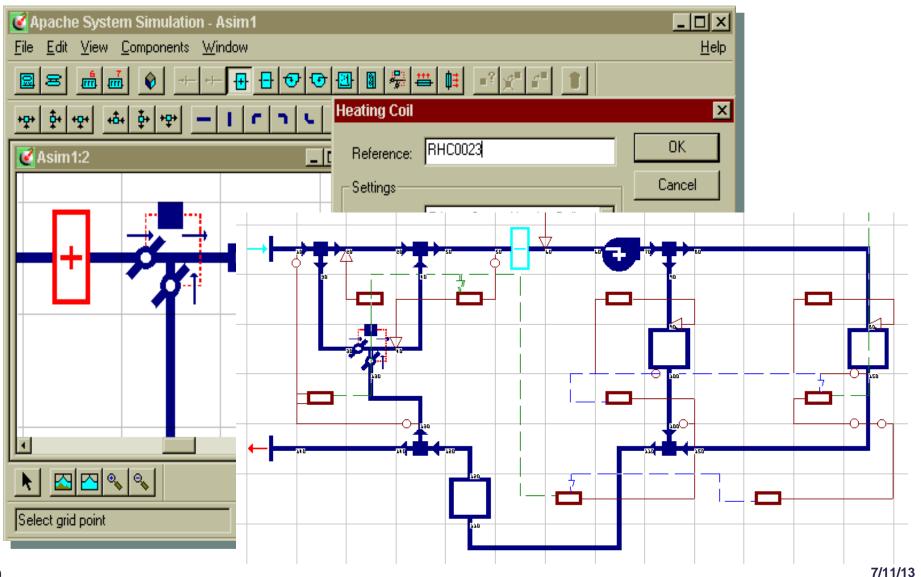








APSIM HVAC System Network and Controls







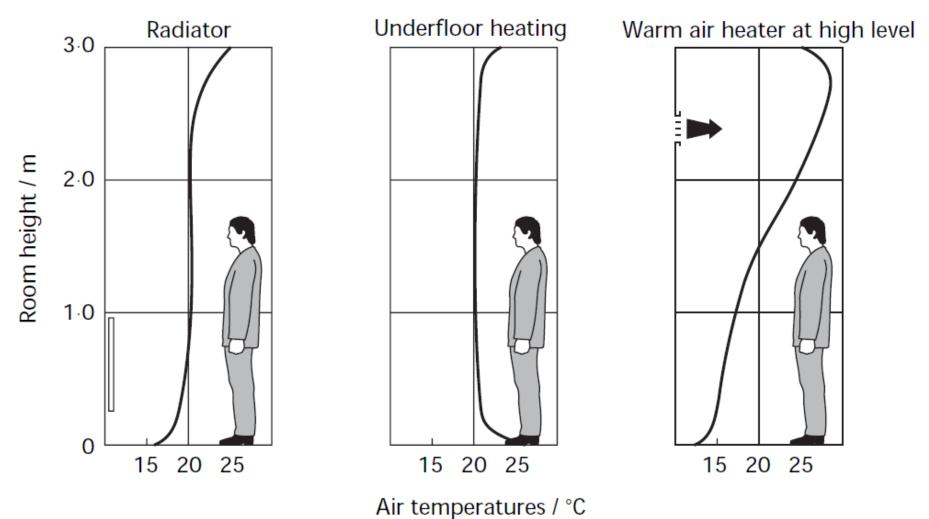
Building Services Engineering



AECOM

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Vertical Air Temperature Distribution with HVAC Systems

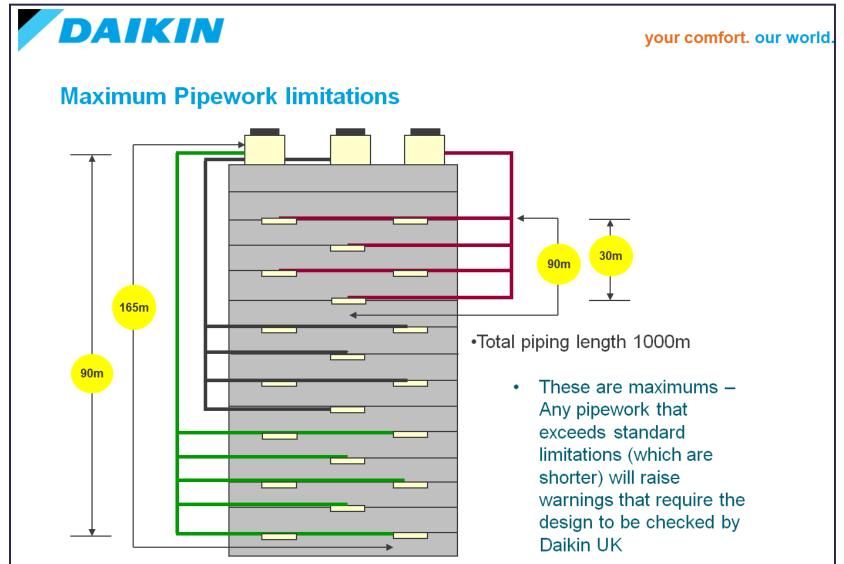


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How Does Cooling Actually Perform

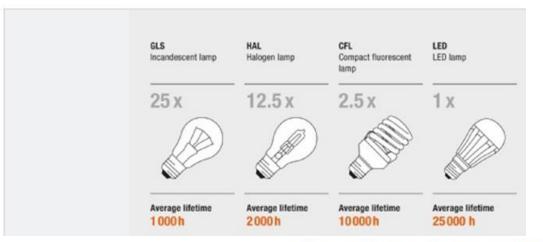




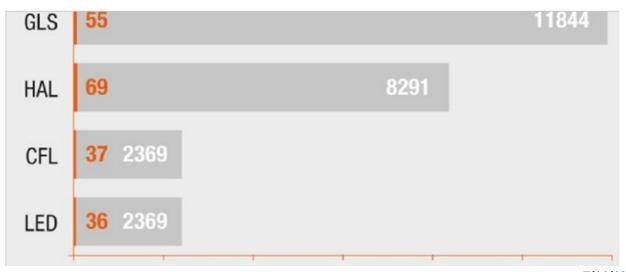


Lighting Equipment and Light Loss Factors

Number of lamps required for 25 000 hours of light



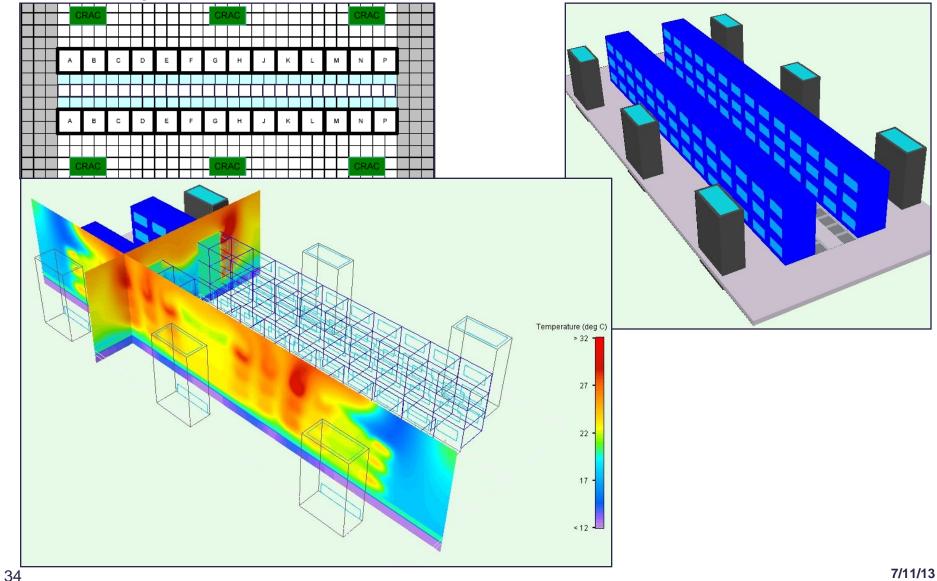
Cumulated Energy Demand based on 25 000 hours of light



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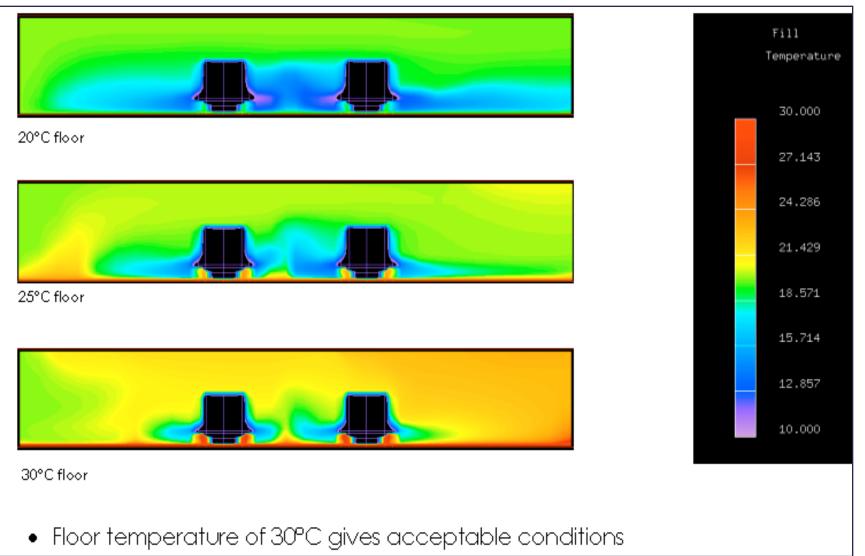
CFD Analyses for Standard Data Centre



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CFD Analysis of Store Food Layout with Underfloor Heating



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Fabric Checks Have a Way to Go!!





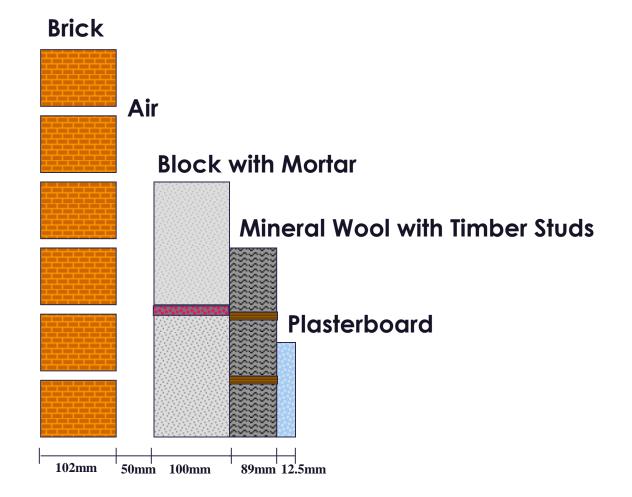
(Hens et. al. 2007)

U Values

		Measured values				
Construction	Calculated	Good workmanship	Poor workmanship			
Full fill Min fibre	0.22	0.22	0.395			
Partial Fill XPS rigid board	0.21	0.24	0.985			



Example – Cavity Wall U-value Calculation







Upper Resistance Limit

Combining these resistances we obtain:

$$R_{upper} = \frac{1}{\frac{F_1}{R_1} + \frac{F_2}{R_2} + \frac{F_3}{R_3} + \frac{F_4}{R_4}} = \frac{1}{\frac{0.818}{3.783} + \frac{0.062}{2.988} + \frac{0.112}{2.126} + \frac{0.008}{1.331}}$$

÷

R1 U-value would be 0.26 W/m²K As most people would

R1 U-value would be 0.30 W/m²K To 1995 proportional area method

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U-value of the Wall

The effect of air gaps or mechanical fixings² should be included in the U-value unless they lead to an adjustment in the U-value of less than 3%.

 $U = 1 / R_T + \Delta U_g$ (if ΔU_g is not less than 3% of $1 / R_T$)

 $U = 1 / R_T$ (if ΔU_g is less than 3% of $1 / R_T$)

In this case $\Delta U_g = 0.003 \text{ W/m}^2\text{K}$ and $1 / R_T = 0.315 \text{ W/m}^2\text{K}$. Since ΔUg is less than 3% of $(1 / R_T)$,

 $U = 1 / R_T = 1 / 3.170 = 0.32$ W/m²K (expressed to two decimal places)

U-value would be 0.26 W/m²K As most people calculate it

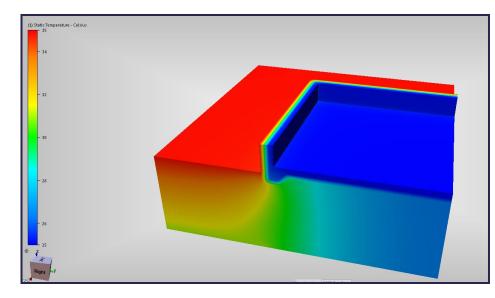
U-value = 0.30 W/m²K for Part L 1995 proportional area method

U-value = 0.32 W/m²K from Part L 2002



Passive House Project Case Study

Super insulation and thermal mass, allow the building envelope to decouple the internal environment from the harsh external conditions



Images shows cut-away of conduction model of wall and ground floor for average summer conditions

the I	Envelope meets or ex recommended by Par Institute					
	Walls and roof	0.09 W/m²K				
	Floor	0.10 W/m²K				
	Glazing	1.00 W/m²K				





CIBSE Guide A10

Vapour Resistivity

Values of vapour resistivity for common materials are given in Table A10.4 under two headings; "minimum" and "typical".

The "minimum" values are the smallest values found in relevant literature^{2,3} and should not be used for general calculations. The "typical" values are taken from the middle of the range of values for each material and may be used for calculation in the absence of more specific data. However, it should be borne in mind that individual samples of material may exceed these typical values by a factor of two or more.





Embodied Energy Data for Aluminium

			Alumin	ium		_	
	Embodie	ed Energy	(EE) Data	base Stati	istics - MJ	/Kg	
Main Material	No. Records	Average EE	Standard Deviation	Minimum EE	Maximum EE	Comments on the Database Statistics:	
Aluminium	111	157.1	104.7	8.0	382.7	Ma	terial Scatter Graph
General	111	157-1	104.7	8-0	382.7		
50% Recycled	4	108.6	53.4	58-0	184.0		
Other Specification	3	146.5	79.3	55.0	193.5	450	
Predominantly Recycled	28	17.9	8.7	8.0	42.9	400 -	*
Unspecified	14	169.1	67.0	68-0	249.9	350-	• • • • •
Virgin	62	224.1	68·5	39-2	382.7	By 300- E	\$0 *
University of Bath			Embo The In Energy	reg Hammond and Craig points is and Peter Ne in the Investory more as to equivalent	d Area and a second sec	(M)/K ³ 300 - 250 - 200 - 150 - 100 - 50 - 0 - 1960	1970 1980 1990 2000 2010 Year of data

C University of Bath





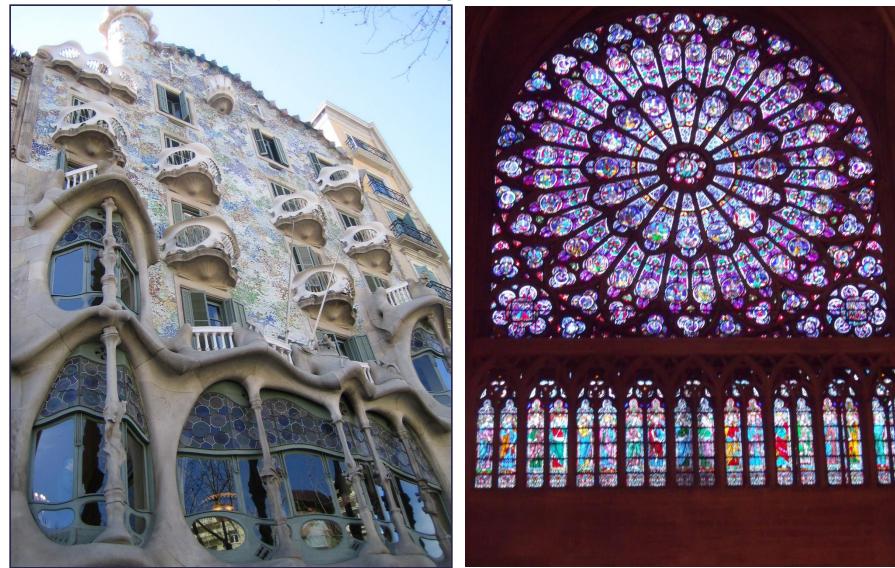
Embodied Energy Data for Glass

			Glass				
	Embodie	d Energy (
Main Material	No. Records	Average EE	Standard Deviation	Minimum EE	Maximum EE	Comments on the Database Statistics:	
Glass	97	20.08	9.13	2.56	62.10		"
Glass, Fibreglass	22	25.58	8.53	11.00	41.81	1 I I	Material Scatter Graph
Market Average	1	30.00	30.00	30.00	-		an an ann an
Predominantly Recycled	2	11.90	11.90	11.90	-	70	
Unspecified	16	26.24	8.41	11.00	41.81		
Virgin	3	24.85	10.25	17.60	32.10	60-	•
Glass, General	75	18.50	8.73	2.56	62.10	The second se	
50% Recycled	1	7.00	7.00	7.00	-	2 50	
Market Average	4	16.81	5.87	12.30	25.09	^{(β} γ/(Σ)	
				bon and		" 60 - 40 - 30 - 20 - Hand energy 10 - 1960	1970 1980 1990 2000 201 Year of data





How Would You Analyse These Façades?







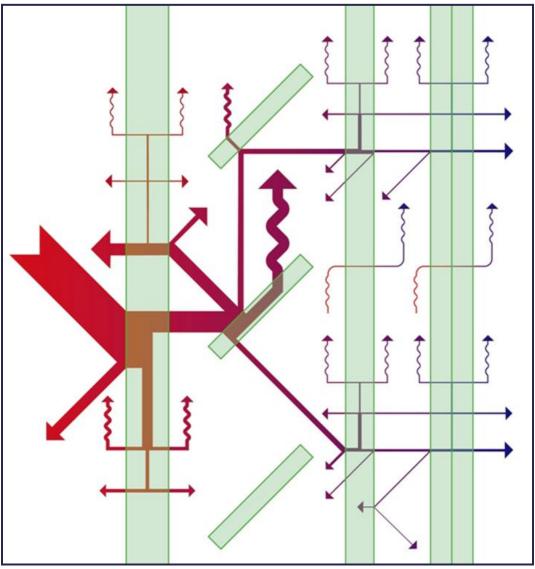
Pilkington Glazing Calculator

〒 ■ ■ ● Ⅰ	u w w		+	U U+I	+ + +	W U	+11 11	I+I				
Glass 1: Pilkington Optifloat^{me} Green 4mm Cavity 1: 16 Gas 1: 90% Argon												
Glass 2: Pilkington Optifloat ^{mer} Clear 8mm V U= 2.6W/M ² K												
13% Light 13% Energy 9% Outside Inside												
Product code	U value	UV%	Light	%		Ener	gy%		Solar factor	Shadi	ng coeff.	
	W/m²K	Tuv	LT	LR out	LR in	ET	ER	EA	g	T SC	S SC	
4gn-16Ar-cl8	2.6	20	71	13	14	45	9	46	0.55	0.64	0.52	
Performance code	Sound reducti	on			Thickness			Weight		Date		
U-value/Light/Energy 2.6/ 71/55		(C;Ctr) (-1 ; -4)				nm 28		kg/ 30		31/01/	2007	

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How Does the Facade Work



How does the Software deal with complex facades

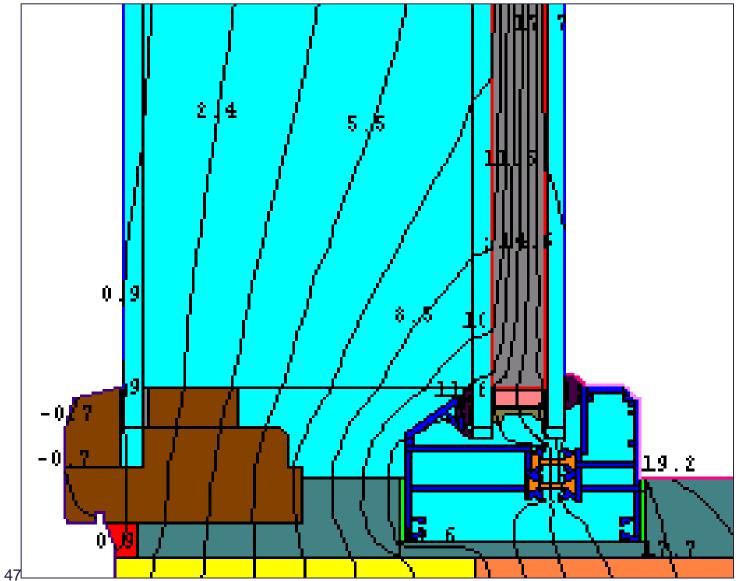
Thanks to Mark Taylor Allies and Morrison

Improving DTM Software









7/11/13

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Technal Fxi Range of Windows

		8 B (0)	1	.9			1.7 1.5			1.2							
		S1	S2	S 3	S4	S1	S2	S3	S 4	S1	S2	S3	S4	S1	S2	S3	S4
	Fixed Light	2.60	2.30	2.30	2.30	2.40	2.20	2.10	2.10	2.30	2.00	2.00	2.00	2.10	1.80	1.80	1.70
FXi46	Open In	2.80	2.50	2.40	2.40	2.70	2.40	2.30	2.30	2.60	2.20	2.20	2.20	2.40	2.00	2.00	2.00
-	Open Out	2.90	2.60	2.50	2.50	2.80	2.50	2.40	2.40	2.70	2.30	2.20	2.20	2.60	2.10	2.10	2.00
	Fixed Light	2.50	2.30	2.30	2.20	2.30	2.10	2.10	2.10	2.20	2.00	2.00	1.90	2.00	1.80	1.70	1.70
FXi52	Open In	2.70	2.40	2.40	2.40	2.60	2.30	2.30	2.30	2.50	2.20	2.10	2.10	2,40	2.00	1.90	1.90
ill.	Open Out	2.80	2.50	2.50	2.50	2.70	2.40	2.30	2:30	2.60	2.30	2.20	2.20	2.50	2.10	2.00	2,00
	Fixed Light	2.30	2.20	2.10	2.10	2.10	2.00	2.00	2.00	2.00	1.80	1.80	1.80	1.90	1.60	1.60	1.60
FXi65	Open In	2.40	2.30	2.20	2.20	2.30	2.10	2.10	2.10	2.20	2.00	1.90	1.90	2.00	1.80	1.70	1.70
. CE	Open Out	2.30	2.20	2.20	2.20	2.20	2.10	2.00	2,00	2.10	1.90	1.90	2.00	1,90	1.70	1.70	1.70

UValue Glass (centre pane)

≤2.2
2.3
2.4
2.5

Size of Window

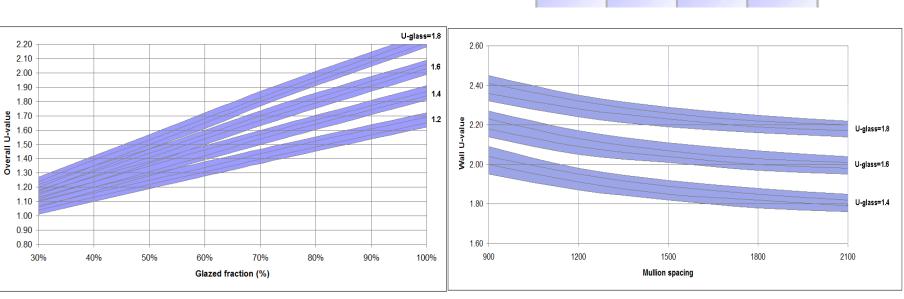
 $SI = 0.75m \times 0.80m$ $S2 = 1.20m \times 1.20m$ $S3 = 1.23m \times 1.48m$

 $S4 = 1.00m \times 2.18m$



- **Calculating rainscreen U-values**
- Inputting data to SBEM





ey height

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CIBSE TM37:2006 – Design for Improved Solar Shading Control

Design for improved solar shading control



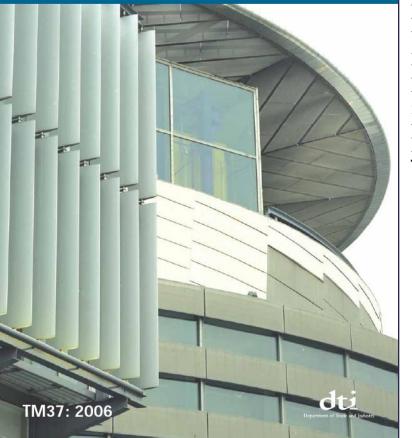


Table 5.4 Weighted average values of $g_{\rm eff}$ for standard 6 mm hard coat low emissivity double glazing with and without blinds

Type of glazing and blind	Value of $g_{\rm eff}$ for stated glazing orientation									
(from outside to inside)	North	NE/NW	E/W	SE/SW	South	Horiz.				
Low-e/clear (no blind)	0.55	0.60	0.62	0.60	0.56	0.61				
Occupant control:										
 low-e/clear, internal blind 	0.52	0.53	0.53	0.51	0.47	0.51				
 low-e/clear, mid-pane blind 	0.49	0.45	0.43	0.41	0.37	0.40				
 low-e/clear, external blind 	0.47	0.41	0.38	0.36	0.33	0.35				
Automatic control with occupant over	erride:									
 low-e/clear, internal blind 	0.52	0.50	0.48	0.46	0.43	0.46				
 low-e/clear, midpane blind 	0.49	0.40	0.34	0.32	0.28	0.29				
 low-e/clear, external blind 	0.47	0.35	0.28	0.25	0.22	0.21				
Fully automatic control:										
 low-e/clear, internal blind 	0.55	0.51	0.48	0.45	0.42	0.44				
 low-e/clear, mid-pane blind 	0.55	0.41	0.33	0.30	0.26	0.26				
 low-e/clear, external blind 	0.55	0.36	0.26	0.23	0.18	0.17				



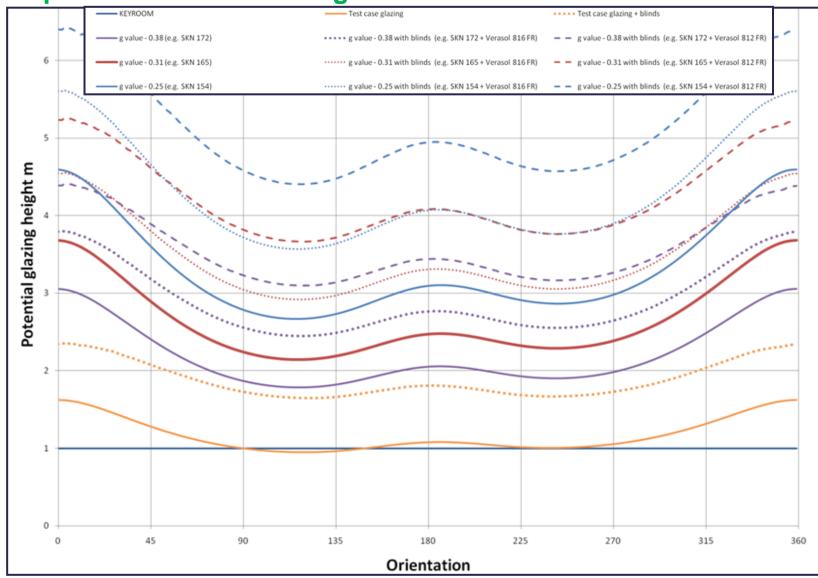
Solar Shading at De Montfort University Business & Law Building







Example for London Showing Benefits of Blinds



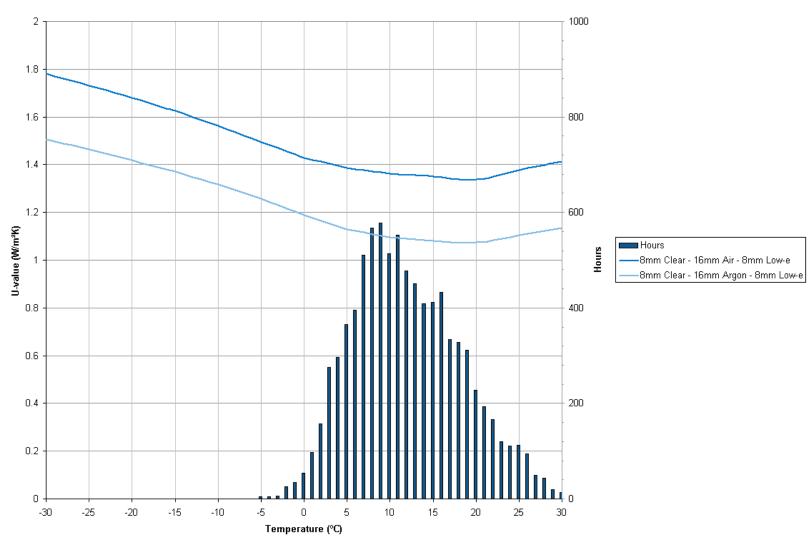
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Outside Air Temperature and U-Values for Glazing

Comparison of centre of pane U-values due to changing temperature (@ 20°C int, 3 m/s wind speed)

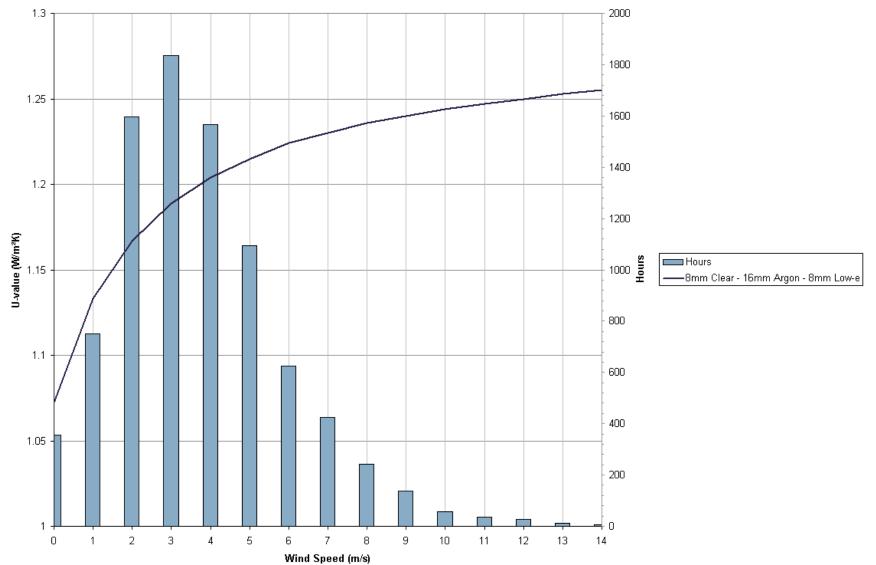


Improving DTM Software





U-value of Glazing and Wind Speed



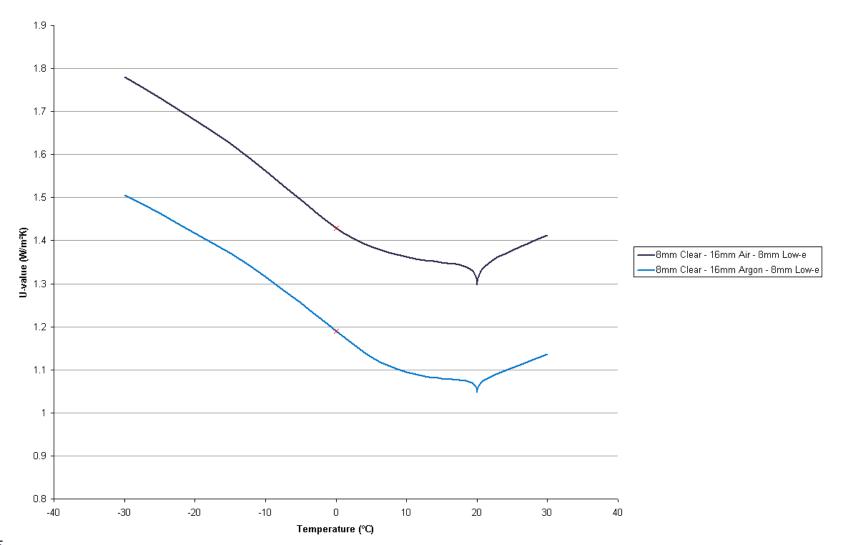
54





Glass Unit U-value with Outside Air Temperature

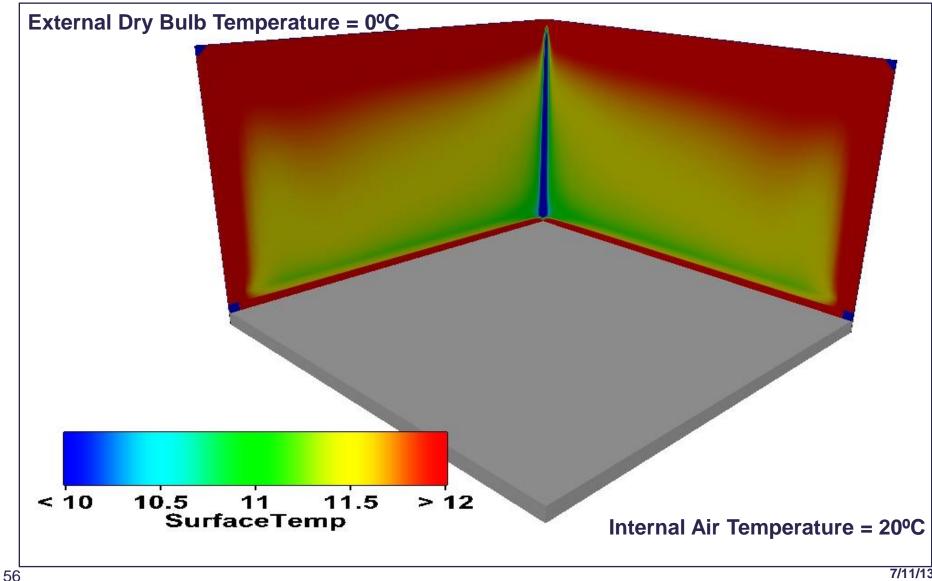
Comparison of U-values due to changing temperature (@ 20°C int, 3 m/s wind speed)







U = 2.2 W/m²K: Glazing Surface Temperatures



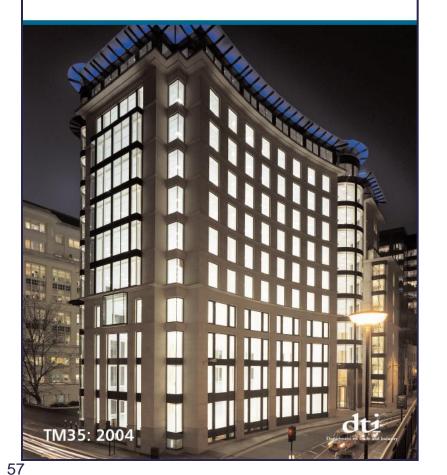
UK GREEN BUILDING COUNCIL God Lega

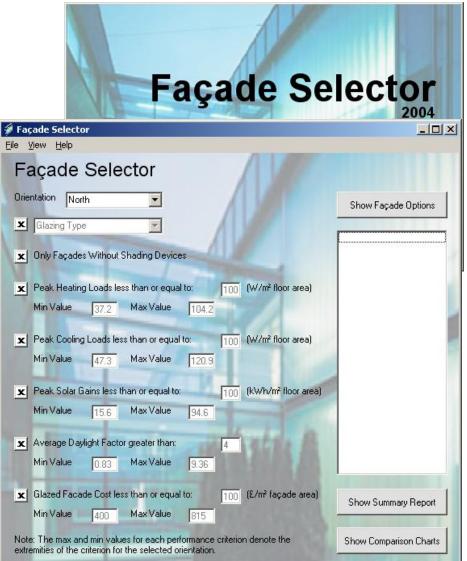


CIBSE TM35:2004 - Façade Selector Toolkit

Environmental performance toolkit for glazed façades









What Should a Roof Look Like? – Photovoltaic's on a Green Sedum Roof







CoolDeck With Phase Change in Stevenage







Improving DTM Software





THANK YOU FOR LISTENING

"If we change the ways you think about building, may be what you build will change the world"

"The earth has no voice.....so someone must speak for it."